

## Determination of Fe–O Bond Energy in Water-gas Shift Catalyst

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**Synopsis.** Oxygen catalyst bond energy may play an important role in determining the catalytic activity in water-gas shift reaction. In the present investigation a method for determining this parameter from electrical conductivity has been suggested.

In view of the fact that water-gas shift reaction in iron(III) oxide catalysts is a typical oxidation-reduction reaction, it is quite obvious that there should exist some correlation between the oxygen catalyst bond energy and shift reaction activity. In case of redox reaction in presence of oxygen this bond energy has been measured by various techniques.<sup>1,2)</sup> But in case of reactions taking place under reducing conditions *e.g.*, water-gas shift reactions, the only reported method is that of Rachkovsky and Yurjeva<sup>3)</sup> who studied the isotope exchange between hydrogen and deuterium oxide on spinels to estimate the oxygen-catalyst bond energy under reducing conditions. In the present investigation a simple method has been suggested to measure this bond energy from electrical conductivity of iron oxide catalyst.

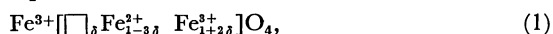
### Experimental

The samples A to E were all shift catalysts of commercial variety containing different type of iron(III) oxides promoted with 7–10% chromium(III) oxide. Sample F is pure iron oxide prepared by precipitation from iron(II) sulfate solution with ammonium carbonate followed by curing in air at 500 °C.

The conductivity cell and the circuit used for measurement have been described in detail in an earlier communication.<sup>4)</sup> Prior to measurement the catalyst was heated to 200 °C in a flow of N<sub>2</sub>+steam in the ratio of 1:5. At 200 °C nitrogen was replaced by hydrogen and the temperature was slowly raised to 350±10 °C. The catalyst was finally stabilized at 460±10 °C. The stabilization was indicated by a constant value of the potential drop. The temperature was slowly brought down to 250 °C and the potential drop was measured at different temperatures after stabilization. Both heating and cooling cycles gave good reproducibility of conductivity values.

### Results and Discussion

On reduction with H<sub>2</sub>+H<sub>2</sub>O mixture the iron oxide catalysts are all reduced to Fe<sub>3</sub>O<sub>4</sub>. In the present investigation it has been observed that all catalysts show good conductivity which means conduction takes place through Fe<sub>3</sub>O<sub>4</sub> phase only irrespective of the presence of chromium(III) oxide. Following Suenaga<sup>5)</sup> and Parravano<sup>6)</sup> the Fe<sub>3</sub>O<sub>4</sub> phase can be assumed to be in oxygen excess nonstoichiometric form which can be represented as:



where  $\square$  is the cation vacancy and  $\delta$  is the mole fraction of cation vacancies and is a measure of the degree

of nonstoichiometry. The conductivity ( $\sigma$ ) at any temperature  $T$  (in K) can then be written as<sup>7)</sup>

$$\sigma = C[1-3\delta][1+2\delta]\exp(-E/RT), \quad (2)$$

where  $C$  is constant and  $E$  is activation energy of conduction. Since  $\delta$  is very small,

$$\sigma = C[1-\delta]\exp(-E/RT). \quad (3)$$

Therefore,

$$\log \sigma = \log C + \log(1-\delta) - \frac{E}{2.303RT}. \quad (4)$$

Let  $\delta_1$ ,  $\delta$ , and  $\sigma_1$ ,  $\sigma$  are the degree of nonstoichiometry and conductivities at temperature  $T_1$  and  $T$  respectively,

Then

$$\log \frac{\sigma_1}{\sigma} = \log \frac{(1-\delta_1)}{(1-\delta)} + \frac{E}{2.303R} \left( \frac{1}{T} - \frac{1}{T_1} \right). \quad (5)$$

If the catalyst is stoichiometric ( $\delta=0$ ) at the temperature  $T$ ,

$$\log \frac{\sigma_1}{\sigma} = \log(1-\delta_1) + \frac{E}{2.303R} \left( \frac{1}{T} - \frac{1}{T_1} \right). \quad (6)$$

From Fig. 1 it can be seen that the plot of  $\log(\sigma_1/\sigma)$  vs.  $(1/T-1/T_1)$  where  $T_1$  is the maximum temperature of measurement *i.e.*, 460±10 °C consists of two parts—linear at lower temperature and nonlinear at higher temperature for all catalysts. The general nature of the conductivity temperature plot obtained for different catalysts is presented in Fig. 2. This shows that the catalyst exhibits variable nonstoichiometry only when  $T > T_s$ . Thus Eq. 5 is obeyed for  $T > T_s$  and Eq. 6 for  $T \leq T_s$ . If the catalyst does not show any variation in stoichiometry throughout the temperature range studied the conductivity temperature relationship can be represented by extrapolating the linear portion corresponding to lower temperature part

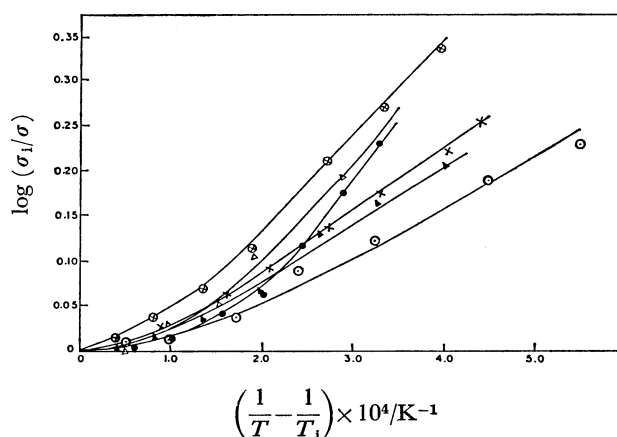


Fig. 1. Variation of resistance of the catalyst with temperature.

Sample A: —△—△—, Sample B: —×—×—, Sample C: —\*—\*—, Sample D: —●—●—, Sample E: —▲—▲—, Sample F: —○—○—.

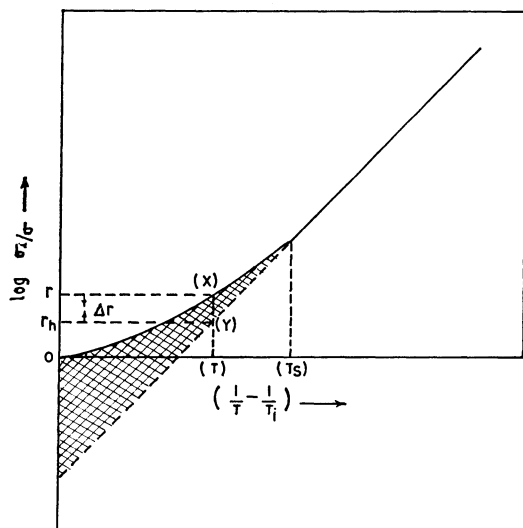


Fig. 2. Change in log (conductivity) vs. (temperature)<sup>-1</sup> plot due to variation in degree of nonstoichiometry.

to higher temperature as shown by the dotted line in Fig. 2. Let  $\sigma$  and  $\sigma_h$  be the conductivities at temperature  $T$  corresponding to points X and Y on the actual curve and on the hypothetical extrapolated line respectively. Since Eq. 5 holds for point X and Eq. 6 for point Y respectively then combining both Eqs. 5 and 6,

$$\log \frac{\sigma_h}{\sigma} = \log \frac{\sigma_1}{\sigma} - \log \frac{\sigma_1}{\sigma_h} = r - r_h = \Delta r$$

$$= -\log(1-\delta), \quad (7)$$

if  $E$  is assumed to be independent of the degree of nonstoichiometry. Such an assumption can be justified on the basis of the reported value of  $E$  for  $\text{Fe}_3\text{O}_4$  and  $\gamma\text{-Fe}_2\text{O}_3$ .<sup>8,9)</sup>

The degree of nonstoichiometry ( $\delta$ ) of an oxide catalyst can be expressed by the following empirical equation.

$$1 - \delta = \left[ \exp \left\{ -\frac{\Delta H}{R} \left( \frac{1}{T_s} - \frac{1}{T} \right) \right\} \right] \left( \frac{p_{\delta_2}^s}{p_{\delta_2}} \right)^{1/2}, \quad (8)$$

where  $\Delta H$  is enthalpy of vacancy formation/mol,  $p_{\delta_2}^s$ ,  $p_{\delta_2}$  are the equilibrium partial pressure of oxygen at temperatures  $T_s$  and  $T$  respectively. When  $T = T_s$ ,  $p_{\delta_2} = p_{\delta_2}^s$ , and  $\delta = 0$ . Since in the present case the partial pressure of oxygen at different temperatures is determined by the dissociation of steam ( $\text{H}_2\text{O} \rightleftharpoons$

TABLE 1. CALCULATION OF OXYGEN CATALYST BOND ENERGY ( $\Delta H$ )  
 $\Delta H_w = 59.3$  kcal/mol,  $T_1 = 460 \pm 10^\circ\text{C}$ .

	Sample					
	A	B	C	D	E	F
$\Delta r$	0.157	0.077	0.053	0.205	0.050	0.100
$(1/T_s - 1/T_1)$ $10^{-4} \text{ K}$	2.9	1.675	1.675	2.475	1.75	4.25
$\Delta H/\text{kcal mol}^{-1}$	61.7	61.0	60.7	63.0	60.5	60.3

$\text{H}_2 + \frac{1}{2}\text{O}_2$ ) we can write

$$\frac{1}{2} \log \left( \frac{p_{\text{O}_2}^s}{p_{\text{O}_2}} \right) = -\frac{\Delta H_w}{2.303R} \left( \frac{1}{T_s} - \frac{1}{T} \right), \quad (9)$$

where  $\Delta H_w$  is the enthalpy of dissociation of steam. Combining Eqs. 7, 8, and 9 and putting  $T = T_1$

$$\Delta r = \frac{1}{2.303R} \left( \frac{1}{T_s} - \frac{1}{T_1} \right) (\Delta H + \Delta H_w). \quad (10)$$

$\Delta H$  for different catalysts has been calculated from Eq. 10 utilizing the values of  $\Delta r$  and  $(1/T_s - 1/T_1)$  from Fig. 1 and are presented in Table 1. The average value of oxygen catalyst bond energy is  $61.6 \pm 2.4$  kcal/mol. Since the adsorption/desorption of each oxygen atom results in formation/rupture of two Fe-O bond, average energy per bond is  $30.8 \pm 1.2$  kcal which is in good agreement with that calculated by Vijh.<sup>10)</sup>

## References

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